



PECASE)TAILORING THE ELECTROMAGNETIC NEAR FIELD WITH PATTERNED SURFACES - NEAR-

**Anthony Grbic
UNIVERSITY OF MICHIGAN**

**12/10/2014
Final Report**

DISTRIBUTION A: Distribution approved for public release.

**Air Force Research Laboratory
AF Office Of Scientific Research (AFOSR)/ RTB
Arlington, Virginia 22203
Air Force Materiel Command**

REPORT DOCUMENTATION PAGE				<i>Form Approved</i> <i>OMB No. 0704-0188</i>	
<small>Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing this collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden to Department of Defense, Washington Headquarters Services, Directorate for Information Operations and Reports (0704-0188), 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302. Respondents should be aware that notwithstanding any other provision of law, no person shall be subject to any penalty for failing to comply with a collection of information if it does not display a currently valid OMB control number. PLEASE DO NOT RETURN YOUR FORM TO THE ABOVE ADDRESS.</small>					
1. REPORT DATE (DD-MM-YYYY)		2. REPORT TYPE		3. DATES COVERED (From - To)	
4. TITLE AND SUBTITLE				5a. CONTRACT NUMBER	
				5b. GRANT NUMBER	
				5c. PROGRAM ELEMENT NUMBER	
6. AUTHOR(S)				5d. PROJECT NUMBER	
				5e. TASK NUMBER	
				5f. WORK UNIT NUMBER	
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES)				8. PERFORMING ORGANIZATION REPORT NUMBER	
9. SPONSORING / MONITORING AGENCY NAME(S) AND ADDRESS(ES)				10. SPONSOR/MONITOR'S ACRONYM(S)	
				11. SPONSOR/MONITOR'S REPORT NUMBER(S)	
12. DISTRIBUTION / AVAILABILITY STATEMENT					
13. SUPPLEMENTARY NOTES					
14. ABSTRACT					
15. SUBJECT TERMS					
16. SECURITY CLASSIFICATION OF:			17. LIMITATION OF ABSTRACT	18. NUMBER OF PAGES	19a. NAME OF RESPONSIBLE PERSON
a. REPORT	b. ABSTRACT	c. THIS PAGE			19b. TELEPHONE NUMBER (include area code)

**Tailoring the Electromagnetic Near Field with Patterned
Surfaces: Near-Field Plates
Final Report FA9550-09-1-0696**

Anthony Grbic

*Department of Electrical Engineering and Computer Science,
University of Michigan,
Ann Arbor, MI, 48109-2122, USA
(Dated: December 5, 2014)*

CONTENTS

I. Objectives	3
II. Near-Field Plates	3
A. Background on Near-Field Plates	3
1. Aperture Fields Supported by a Near-Field Plate	4
B. Work Performed and Accomplishments	7
1. Experimental Verification	7
2. Analytical Investigation of Near-Field Plates	8
3. Corrugated Near-Field Plates	8
4. Near-Field Plates as High-Resolution Probes	9
5. Generating Bessel Beams with Near-Field Plates	9
6. Planar Near-Field Plates	10
7. Unidirectional Near-Field Plates	11
8. Near-Field Plates for Wireless Non-Radiative Power Transfer	11
C. Impact	12
III. Controlling Electromagnetic Fields with Anisotropic and Inhomogeneous Metamaterials	13
A. Overview	13
B. Work Performed and Accomplishments	13
1. Tensor Transmission-Line Metamaterials	13
2. Homogenization of Tensor Transmission-Line Metamaterials	14
3. Alternative Material Parameters for Transformation Electromagnetics Designs	15
4. A Transformation-Designed Device Implemented with Tensor Transmission-Line Metamaterials	15
5. Tailoring the Phase and Power Flow of Electromagnetic Fields with Metamaterials	15
C. Impact	16
IV. Personnel Supported	17
V. Publications	18
A. Journal Papers	18
B. Letters	19
C. Conference Papers	20
References	25

I. OBJECTIVES

The primary objective of the proposed work was to theoretically and experimentally investigate near-field plates and their potential uses. Near-field plates are subwavelength-textured surfaces that can focus electromagnetic fields to deep subwavelength resolutions. Their operation was theoretically explained, design methodologies were formulated, and various prototypes developed at microwave frequencies.

A second objective also emerged during the course of this research work. The second objective was rather broad: to arbitrarily control electromagnetic fields within a 2D region of space using anisotropic and inhomogeneous metamaterials. This effort involved the development of circuit-based metamaterials that exhibit tensorial effective material parameters, and the implementation of electromagnetic devices using such metamaterials. It also included the development of synthesis methods for anisotropic and inhomogeneous 2D metamaterials.

II. NEAR-FIELD PLATES

This section describes research work related to the primary objective of developing near-field plates: textured surfaces that allow subwavelength control over the electromagnetic near field.

A. Background on Near-Field Plates

During the past decade, there has been strong interest in the development and characterization of electromagnetic metamaterials, as well as their practical application. Metamaterials are materials engineered at a subwavelength scale to exhibit tailored electromagnetic properties. Their electromagnetic properties are derived from their subwavelength structure/granularity, rather than solely their constitutive materials. Interest in metamaterials surged with the development of a metamaterial exhibiting a negative index of refraction [1] in 2001. One of the first metamaterial devices that intrigued the scientific community and drew widespread attention was the "perfect lens" introduced by John B. Pendry in [2]. This seminal work set off the scientific and engineering community's quest for the superlens: a lens capable of subwavelength resolution [3]. A superlens is a slab with negative material parameters (negative permittivity and permeability) that can manipulate the near field and focus electromagnetic waves to resolutions beyond the diffraction limit. Since Pendry's theoretical proposal [2], numerous superlenses have been implemented at frequencies ranging from the radio frequency (RF) to the optical spectrum [4–8].

An alternative approach to subwavelength focusing was introduced by the PI and his collaborator Roberto Merlin in 2007 [9, 10], and experimentally verified in 2008 [11]. This new approach relies on subwavelength-structured, grating-like surfaces rather than volumetric structures (slabs). These devices have been referred to by a number of names including near-field plates [9–16] and evanescent field lenses [9], and later as holographic screens [17], metascreens [18] and spatially beam shifted transmission screens [19]. In this report, they will be collectively referred to as near-field plates. These planar structures can focus electromagnetic waves beyond the diffraction limit, but are simpler to fabricate than the volumetric metamaterial superlenses. They do not require 3D fabrication, but rather only single layer processing.

Near-field plates can be viewed as metamaterial surfaces (metasurfaces or metafilms) [20]. They are textured/structured at a subwavelength scale, in the same way that volumetric metamaterials exhibit subwavelength granularity. They can be described macroscopically in terms of effective impedances, just as volumetric metamaterials are described in terms of effective material parameters: permittivity and permeability. In the most general sense, a near-field plate is a collection/array of closely spaced, non-periodically varying scatterers (polarizable particles, impedance elements, small antennas) that, when excited, strongly interact to produce a desired subwavelength focal pattern. A near-field plate can take on various forms. It can be a non-periodic surface or array of polarizable particles that is excited by an incident field [10–12, 18, 19], a directly fed array of subwavelength antennas, or a driven subwavelength antenna element surrounded by parasitic radiators [13–15, 21–23]. In all these cases, a highly oscillatory field is excited at the surface of the near-field plate which converges to a subwavelength pattern at a near-field focal distance [24].

Antenna engineers typically deal with wireless systems that operate at large distances, and therefore contend with far-field radiation and pattern synthesis. The near field of an antenna is generally considered a nuisance that causes undesired effects such as mutual coupling between antenna elements or interactions with the platform onto which the antenna is mounted. In contrast, near-field microscopists deal with length scales at the other extreme; those that are subwavelength. In near-field microscopy, subwavelength focal spots or field patterns, needed for high-resolution imaging, are produced by placing subwavelength probes (tapered waveguide apertures, dielectric and metallic tips) in close proximity to the sample being imaged [25, 26]. In this way, detection over a subwavelength area of the sample is achieved. In near-field plate design, pattern synthesis techniques are applied at a near-field operating distance. So length scales are close to those in near-field microscopy, but the design techniques are reminiscent of those employed in antenna design.

Near-field plates provide some distinct advantages over conventional probes used to confine/localize electromagnetic field to subwavelength spots, such as the electrically small apertures used in near-field microscopy [25]. Firstly, the shape of the subwavelength focal pattern can be tailored by simply changing the design of the plate. In other words, near-field plates allow one to manipulate and sculpt the electromagnetic near field. In addition, near-field plates can have a larger operating distance than conventional probes (electrically small apertures). The operating distance can be defined as the distance at which the subwavelength focus is formed. The electromagnetic field scattered or emitted by an electrically-small aperture diverges quickly away from it. In contrast, the highly oscillatory currents on a near-field plate confine the field and prevent it from diverging over a near-field focal length [9]. This allows a subwavelength focal spot to be maintained at a larger operating distance, or alternatively allows a smaller focal spot than could be achieved using a conventional probe at a fixed distance [11].

1. Aperture Fields Supported by a Near-Field Plate

To gain an understanding of near-field plates, as well as the near-field patterns they produce, let us consider one of the simplest near-field plates possible. A linear near-field plate is shown in Fig. 1, which can create a subwavelength line (1D) focus when excited by an electromagnetic source/incident wave. The depicted plate is invariant in the x direction, so the depicted geometry is two dimensional. For simplicity, let's consider the electric-field

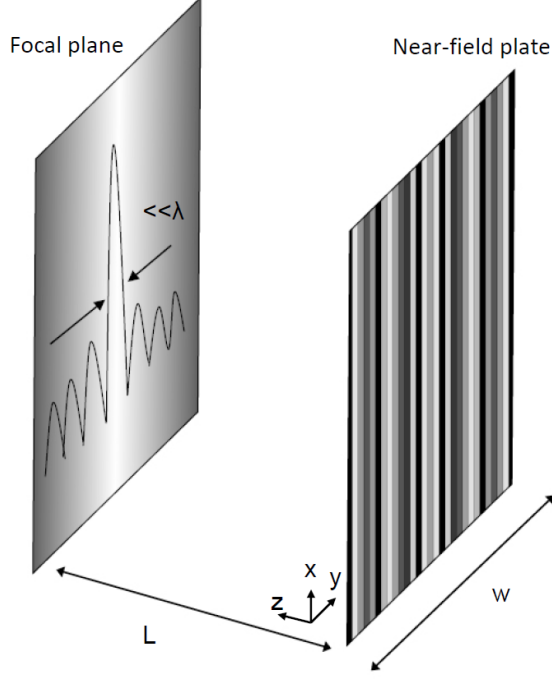


FIG. 1. A schematic showing a near-field plate ($z = 0$) and its focal plane ($z = L$). A near-field plate is a non-periodic, planar device that can focus electromagnetic field to spots or lines of arbitrary subwavelength dimension. The near-field plate's non-periodic impedance variation is graphically represented by its shading.

focus to be an s -polarized sinc function of the following form:

$$\vec{E}_{focal}(y, z = L) = E_0 \frac{\sin(q_0 y)}{q_0 y} \hat{x} = E_0 \text{sinc}(q_0 y) \hat{x} \quad (1)$$

at a focal distance $z = L$ from the plate. The focus is plotted in Fig. 2(a) for a value of $q_0 = 10k_0$, where $k_0 = 2\pi/\lambda$ is the free space wavenumber. To find the general form of the aperture field (electric field at the surface of the near-field plate) needed to produce the subwavelength focus, we will simplify the problem and assume that the plate is infinite in extent ($W \rightarrow \infty$). By Fourier transforming the focal pattern, its spectral representation can be found

$$\vec{E}_{focal}(k_y) = E_0 \frac{\pi}{q_0} \Pi(k_y, q_0) \hat{x}, \quad (2)$$

where $\Pi(k_y, q_0)$ is the rectangular function with amplitude one, extending from $k_y = -q_0$ to $k_y = q_0$ in the spectral domain (see Fig. 2(b)). Back-propagating this spectrum (phase reversing the propagating spectrum and growing the evanescent spectrum from the focal plane to the plate's surface) and then inverse Fourier transforming (IFT) it, the aperture field at the surface of the plate can be obtained [10, 16],

$$\begin{aligned} \vec{E}_{ap}(y) &= \mathcal{F}^{-1}\{\vec{E}_{ap}(k_y)\} = \\ &\mathcal{F}^{-1}\left\{E_0 \frac{\pi}{q_0} e^{jk_z L} \Pi(k_y, q_0)\right\} \hat{x}, \end{aligned} \quad (3)$$

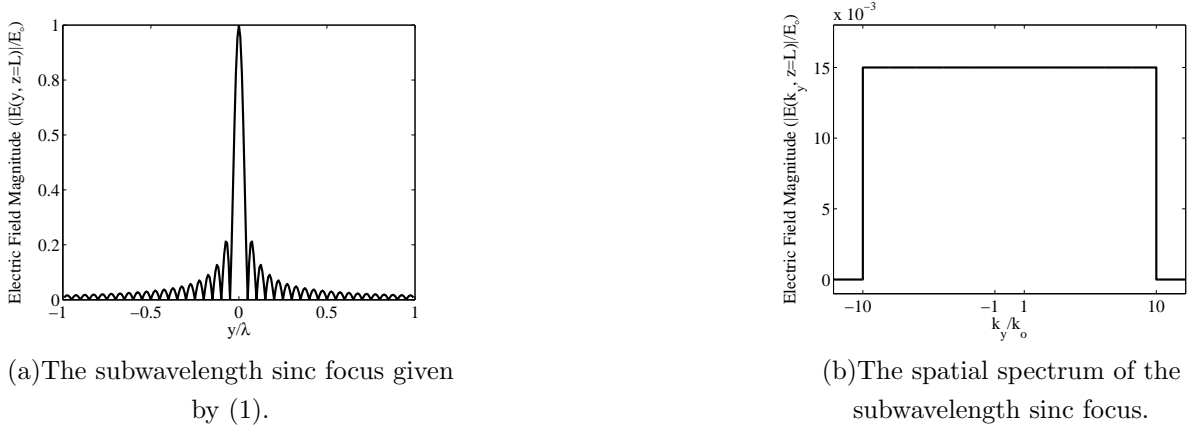


FIG. 2. The subwavelength sinc focus ($q_0 = 10k_0$) and its spectral representation.

where the symbol \mathcal{F}^{-1} denotes the IFT with respect to transverse wavenumber k_y , and k_z is the wavenumber in the z direction defined as:

$$k_z = \begin{cases} \sqrt{k_0^2 - k_y^2} & : k_y^2 < k_0^2 \\ -j\sqrt{k_y^2 - k_0^2} & : k_y^2 > k_0^2 \end{cases}. \quad (4)$$

For near-field plates that focus electromagnetic waves to subwavelength resolutions ($q_0 \gg k_0$), the following quasi-static approximation can be applied [16]

$$\sqrt{k_0^2 - k_y^2} \approx -j|k_y| \quad (5)$$

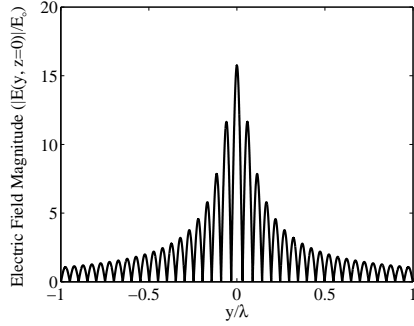
and the field at the plate simplified to the following approximate expression [10]

$$\vec{E}_{ap}(y) \approx \frac{E_0 e^{q_0 L} [L \cos(q_0 y) + y \sin(q_0 y)]}{q_0 (y^2 + L^2)} \hat{x}. \quad (6)$$

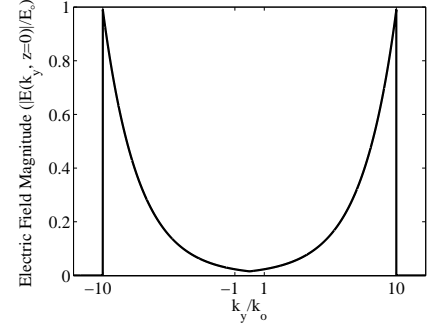
This field is highly oscillatory and has high evanescent field content. The aperture field needed to produce the focus shown in Fig. 2(a) is plotted in Fig. 3(a), where it is assumed that $L = \lambda/15$ and $q_0 = 10k_0$. The aperture field's spectrum is shown in Fig. 3(b), which clearly illustrates the dominance of the evanescent spectrum ($k_y > k_0$). Back-propagating the focal pattern from the focal plane to the plate's surface leads to an evanescent spectrum which exponentially increases with transverse wavenumber (k_y) [16]. In the quasi-static limit, the imaginary poles $\pm jL$ of the aperture field (see (6)) identify the near-field plate's focal length L [9]. In addition, the period of the highly oscillatory field along the plate (aperture field), characterized by the maximum wavenumber q_0 , defines the resolution of the focus. For example, the null-to-null beamwidth of the focal pattern given by (1) is

$$\Delta y = \frac{2\pi}{q_0}. \quad (7)$$

These two properties of the aperture field, the imaginary poles which define the focal length and period of oscillation which determines resolution, are universal to all near-field plates [9].



(a) The aperture field given by (6).



(b) The spatial spectrum of the aperture field given by (6).

FIG. 3. The aperture field needed to produce the subwavelength focus shown in Fig. 2 and its spectral representation.

B. Work Performed and Accomplishments

This section summarizes the work that was performed under the Presidential Early Career Award for Scientists and Engineers (PECASE). The grant supported the development of a novel approach to subwavelength focusing using non-periodic, patterned surfaces. As noted, these patterned surfaces, referred to as near-field plates, were co-invented by the Principal Investigator (PI) and his collaborator, Roberto Merlin, at the University of Michigan. Roberto Merlin proposed a general class of aperture field distributions that can form a subwavelength focus at a prescribed focal plane in the aperture's reactive near field [9]. The PI's research group developed completely passive surfaces (near-field plates) that can achieve the desired aperture fields. In addition, the PI and his group outlined a detailed design procedure: explaining how to synthesize a near-field plate to produce a desired subwavelength focal pattern. Using this synthesis procedure, a number of prototypes were developed and experimentally verified. The advances achieved during the duration of the grant are outlined below. For a more in-depth description, the reader is referred to the Ph.D. dissertation of Dr. Mohammadreza F. Imani, the PI's former doctoral student [27].

1. Experimental Verification

Initially, the PI and his group devised a proof-of-concept near-field plate at microwave frequencies [10], and experimentally verified its ability to focus microwave radiation to sub-wavelength resolutions [11]. The near-field plate consisted of only capacitive elements and focused microwaves emanating from a cylindrical source to line focus (see Fig. 4). In experiment, a focus that is an eighteenth of a wavelength in size was formed by the plate. This focus is 6.5 times smaller than could be achieved using a conventional lens. Results of this initial study were reported in the journal Science [11].

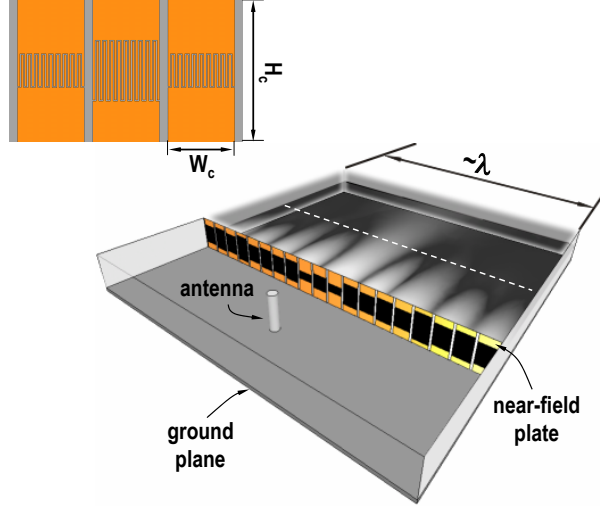


FIG. 4. Schematic showing the experimental set-up for testing the first near-field plate. The figure shows a dipole antenna (cylindrical source) and near-field plate inside a parallel plate waveguide. The top ground plane has been removed for clarity. The near-field plate consists of an array of interdigitated capacitors printed on an electrically-thin microwave substrate. Also shown is a contour plot of the electric field on the image side (logarithmic scale). The dashed white line denotes the focal plane. The three central interdigitated capacitors of the near-field plate are shown in the inset: $H_c = 15.0$ mm, $W_c = 7.5$ mm.

2. Analytical Investigation of Near-Field Plates

An analytical study of near-field plates by the PI's group provided insight into the design and operation of near-field plates [16]. The analysis highlighted the characteristic features of the current density and electromagnetic fields at the surface of near-field plates, and theoretically proved that these devices can be realized using purely reactive surfaces. It also showed how the electromagnetic fields change, both in the spatial and spectral domains, as they propagate from the plate's surface to the focal plane. These analytical results [16] were used to illustrate the similarities and differences between near-field plates and existing near-field focusing devices such as metamaterial slabs with negative material parameters.

3. Corrugated Near-Field Plates

Corrugated near-field plates were also developed as part of this research effort. In contrast to the initial design [11], which relied on illuminating sheets of printed circuit elements to create the desired focus, the new near-field plates relied on subwavelength grooves (corrugations) of varying depth which surround an central aperture to create the desired focus [13, 14, 21], as shown in Fig. 5. These new designs (referred to as "corrugated near-field plates") represent an important alternative to the patterned-surface near-field plates. The patterned-surface implementations were excited by a free-space wave, while the corrugated surfaces were directly fed by a coaxial waveguide, eliminating free-space path loss and improving the efficiency of coupling power from the source to the focus.

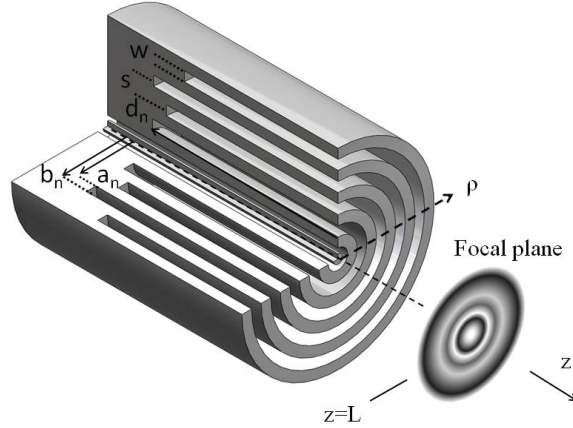


FIG. 5. A concentrically corrugated near-field plate. The focal spot is shown at a distance $z = L$ from the surface of the near-field plate

4. Near-Field Plates as High-Resolution Probes

The experimental verification of a concentrically corrugated near-field plate constituted a major step forward in establishing the near-field plate concept as a practical means for tailoring near-field electromagnetics [21]. The developed near-field plate (see Fig. 5) was the first to produce a two-dimensional subwavelength focal pattern. The beam emitted by the corrugated near-field plate was significantly narrower than that emitted by the conventional coaxial probe, thus confirming the near-field plate's superior ability to confine electromagnetic field over a focal length (an extended operating distance). The corrugated near-field plate was used to image two coaxial sources placed a subwavelength distance apart. The images obtained using the near-field plate exhibited significantly higher resolution than those obtained using the coaxial probe alone [21]. The research results demonstrated that non-periodic, concentrically corrugated surfaces can provide new opportunities to develop high-resolution near-field probes and sensors.

5. Generating Bessel Beams with Near-Field Plates

Concentrically corrugated near-field plate which can generate evanescent Bessel beams at microwave frequencies were also developed [28]. The generation of evanescent Bessel beam was verified through full-wave simulation of the proposed near-field plate. The near-field plate consisted of nonperiodic concentric corrugations that surround a coaxially fed aperture. The performance of the near-field plate was contrasted against a coaxial probe and a near-field plate designed to produce an Airy focal pattern with the same beamwidth. In contrast to earlier methods of generating evanescent Bessel beams that were elaborate and bulky, and often only produced propagating Bessel beams, the near-field plate approach is straightforward and allows flexibility over the properties of the generated beam. For example, the inevitable truncation of Bessel beams can be tailored using the near-field plate approach [28]. The truncation of the Bessel beam has a significant impact on the beam performance: a wide truncation results in a beam that can retain its shape over a larger range, while a narrow truncation results in a short range. On the other hand, a smaller near-field plate is required to generate an evanescent Bessel beam truncated by a narrow truncation. We



FIG. 6. A planar near-field plate which consists of concentric annular slots on a circular grounded dielectric slab. The plate is excited through a coaxial cable and its rim is short circuited. The slots are loaded with lumped element impedances designed to produce a prescribed subwavelength focal pattern. (a) Side view. (b) Front view.

believe this simple and effective near-field plate approach to generating evanescent Bessel beams will find application in many areas such as near-field imaging/probing systems, high-resolution data storage, and medical targeting devices.

6. Planar Near-Field Plates

We have designed, fabricated, and measured planar near-field plates [29]. In contrast to earlier near-field plate designs, these surfaces can be directly fed through a connector and fabricated using standard printed circuit board technology. The plates consist of concentric annular slots on a circular grounded dielectric slab excited through a coaxial connector, as shown in Fig. 6. The annular slots are loaded with lumped element impedances which are designed to produce a prescribed subwavelength focal pattern.

A step-by-step procedure for designing these plates was introduced. Different near-field plates were designed to highlight the ability of near-field plates to produce various patterns. Two different near-field plates were designed to generate evanescent Bessel beams of different beamwidths, and a third one was designed to generate an Airy pattern. The proposed structures were fabricated using printed circuit board technology. The fabricated plates were shown to produce near-field patterns in close agreement with simulation, thereby experimentally verifying their design and operation. Furthermore, the Bessel beam near-field plates were experimentally demonstrated to produce a beam with nearly fixed shape and subwavelength beamwidth over a near-field distance. Over the same distance, neither the beamwidth nor the shape were preserved by the near-field plate that produced the Airy pattern.

The proposed near-field plates are planar, easy to fabricate and feed, and are robust to losses. Their planar design makes them amenable for integration with electronics. Given these promising characteristics, we believe these plates will emerge as practical means for tailoring the electromagnetic near field. They will find application in several areas such as high-resolution imaging and probing, biomedical targeting devices, as well as wireless power

transfer devices.

7. *Unidirectional Near-Field Plates*

We developed a method for creating unidirectional, subwavelength electromagnetic near-field patterns [30]. Specifically, we devised near-field plates, which can form prescribed, unidirectional near-field patterns of subwavelength resolution. Earlier near-field plates demonstrated extreme field tailoring capabilities. However, their performance suffered from radiation/reflection into undesired directions; those other than the subwavelength focus. This hampered the performance of near-field plates, limiting their practical use. We addressed this long-standing issue by devising unidirectional near-field plates that can form a subwavelength focal pattern, while suppressing the field scattered/reflected in the backward direction. The design and operation of the unidirectional near-field plates was verified through full-wave simulation. Unidirectional near-field plates may find application in high-resolution imaging and probing, lithography systems, high-density data storage, electromagnetic targeting devices for biomedical applications, and wireless non-radiative power transfer systems. As an example, a unidirectional near-field plate's utility as a high-resolution probe was demonstrated through full-wave electromagnetic simulation.

8. *Near-Field Plates for Wireless Non-Radiative Power Transfer*

A near-field plate consisting of arrays of loops was developed for use in wireless non-radiative power transfer systems [31]. Specifically, a near-field plate was designed to replace the transmitting coil in current wireless non-radiative power transfer systems. The field emitted by coils in current systems form broad, dipole magnetic field patterns [32]. The goal was to develop near-field plates (arrays of subwavelength loops) that suppress radiation in unwanted directions and at far distances from the transmitter, while maintaining near-field coupling in the intended direction for high efficiency wireless power transmission.

We have demonstrated a highly efficient unidirectional wireless power transfer using near-field plates. The proposed near-field plate consisted of an array of loops placed close to the transmitting loop of a wireless power transfer system. The loops of the near-field plate were loaded with specified impedances to form a desired unidirectional near-field pattern. The step-by-step procedure to design such device was outlined. It was shown that the currents on the near-field plate can be adjusted such that the near-field plate and the transmitting loop interfere constructively in the forward direction (toward the receiver) and destructively in other directions, thus forming a unidirectional near-field pattern. Furthermore, the combined power leaked to the far field was reduced. Two different near-field plates were shown in fullwave simulation and experiment to be able to maintain a high power efficiency (comparable to existing technologies) while significantly suppressing the power leaked into unwanted directions. The proposed near-field plate can find application in many scientific, biomedical, security, and commercial devices to reduce health concerns, interference, and metering and detection problems.

C. Impact

Near-field probes and subwavelength focusing devices based on near-field plates, capable of generating subwavelength beam waists and focal patterns, will find numerous applications. Research on near-field plates may lead to advances in biomedical devices, microscopes with unprecedented resolution, lithography systems that allow unparalleled levels of electronic integration, as well as possible improvements to existing wireless power transfer systems.

The near-field plate's ability to manipulate the near field and provide strong spatial confinement could be leveraged to improve the performance of near-field sensors. High-resolution probes have already been developed for near-field microwave microscopy [13, 14, 21–23]. The subwavelength focus formed by a near-field plate when transmitting, allows it to detect over the same narrow spot when used as a receiver or probe. For microscopy applications, the availability of sub-micron and sub-nanometer feature fabrication techniques could allow arbitrarily high resolutions.

Near-field plates may also find use in wireless non-radiative power transfer systems. Specifically, megahertz receiving and transmitting devices based on near-field plates could provide specific advantages over the resonant coils that have been used to date [33]. Near-field plates could be designed to provide magnetic field illumination to only certain areas of a confined environment, where electronic devices are typically placed. For example, tailored "energy hotspots" could be established on the tops of desks or counter tops using near-field plates. Near-field plates may also radiate less energy to the far field than single or multi-turn loops due to the oscillatory (in and out-of-phase) currents supported by them.

Near-field plates could conceivably be used to improve targeting capabilities in medical devices such as those used in transcranial magnetic stimulation (TMS) [34]. Specifically, the use of near-field plates may lead to increased electromagnetic field penetration while still maintaining a small stimulated volume within the brain. In TMS, a time-varying magnetic field is used to induce an electromotive force within brain tissue in order to excite neurons. The super-resolving power of a near-field plate could perhaps be used to precisely direct neuronal stimulation in TMS.

At optical frequencies, near-field plates can be realized using plasmonic (inductive) and dielectric (capacitive) materials [35–40]. The microwave near-field plate designs reported could also be extended to optical frequencies using the concept of nanocircuit elements [41]. Nanostructured implementations hold promise for near-field optical data storage [42], near-field microscopy and lithography applications. Near-field plates could also be integrated into quasi-optical and optical systems as focusing or beam-shaping elements. For example, an incident beam could be focused to sub-wavelength spots (waists) prior to entering a millimeter-wave, THz, infrared or optical device. In this way, the size of system components could be significantly reduced. Such focusing elements could be used as light concentrators in infrared or optical detector arrays. Near-field plates could also be employed as beam-shaping devices. For instance, near-field plates have been used to generate Bessel beams.

III. CONTROLLING ELECTROMAGNETIC FIELDS WITH ANISOTROPIC AND INHOMOGENEOUS METAMATERIALS

A. Overview

This section covers research work related to the second research objective: arbitrarily controlling fields in a 2D space through electromagnetic anisotropy and inhomogeneity. This work began with the development of circuit-based metamaterials that exhibit tensorial effective material parameters, referred to as tensor transmission-line metamaterials. These metamaterials opened new opportunities in the development of planar transformation electromagnetics devices [43]. Homogenization methods were developed for tensor transmission-line metamaterials and they were used to realize a beam-shifting slab: a transformation electromagnetics device. The homogenization work resulted in methods to find alternative material parameters for transformation electromagnetics devices [43], and the development of synthesis methods for anisotropic and inhomogeneous media. These efforts are elaborated on in the following sections. For a more in-depth description, the reader is referred to the Ph.D. dissertation of Dr. Gurkan Gok, the PI's former doctoral student [44].

B. Work Performed and Accomplishments

This effort on arbitrarily controlling fields in a 2D space through electromagnetic anisotropy and inhomogeneity evolved over the course of this grant. The following subsections describe the work performed and contributions, in the sequence that they occurred.

1. *Tensor Transmission-Line Metamaterials*

The PI introduced tensor transmission-line metamaterials: a new class of metamaterials exhibiting tensorial effective material parameters, low losses and broad bandwidths of operation [45]. Tensor transmission-line metamaterials present a circuit-based approach to designing anisotropic and inhomogeneous media. They provide a one-to-one equivalence between material parameter tensors and circuit parameters, as shown in Fig. 7. In contrast to earlier works [4, 46–53], these transmission-line metamaterials can possess off-diagonal effective material parameters, while still maintaining a uniform rectangular unit cell. A circuit schematic of a tensor transmission-line metamaterial unit cell is shown in Fig. 8(a). A representative planar implementation of a tensor transmission-line unit cell is depicted in Fig. 8(b).

In this work, an approximate tensor analysis of the proposed metamaterials was developed. Bloch analysis was also carried out to verify the approximate analysis and derive exact dispersion equations and impedance relations. Finally, simulation results were presented that validated the analysis and showed the utility of this new class of metamaterials. The propagation characteristics of tensor transmission-line (TL) metamaterials were subsequently verified through full-wave analysis [54]. The ability to design tensor metamaterials such as these is important to the practical implementation of novel devices derived through transformation optics/electromagnetics.

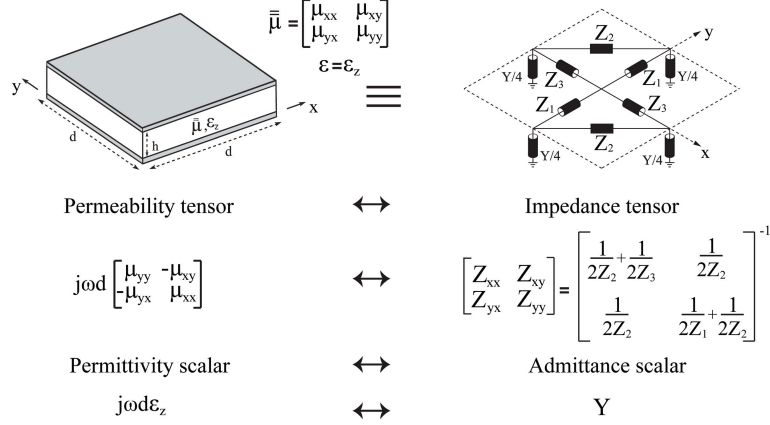


FIG. 7. The one-to-one relationship between material parameters of a magnetically anisotropic medium and the circuit quantities in tensor transmission-line metamaterials.



FIG. 8. Tensor transmission-line (TL) metamaterial unit cells (a) A circuit schematic of a tensor TL unit cell (b) A printed, tensor TL unit cell implemented using standard printed circuit board technology: printed traces over a grounded dielectric substrate.

2. Homogenization of Tensor Transmission-Line Metamaterials

After the introduction of tensor transmission-line metamaterials, a rigorous method for homogenizing these metamaterials was developed. Tensor transmission-line metamaterials consist of loaded transmission-line networks, that can possess magnetically anisotropic (tensor) effective material parameters. The developed homogenization employs a local field averaging procedure to compute the anisotropic effective material parameters. The material parameters can be dispersive or non-dispersive. For the tensor metamaterials possessing dispersive effective material parameters, the homogenization method takes advantage of the circuit topology of tensor transmission-line metamaterials to predict material parameters over a frequency range. The developed homogenization method was essential to characterizing and designing tensor transmission-line metamaterials that can be fabricated using standard printed circuit board techniques, and used to design planar transformation electromagnetics microwave devices.

3. *Alternative Material Parameters for Transformation Electromagnetics Designs*

The development of the homogenization process for tensor transmission-line metamaterials inadvertently led to a second discovery: a formulation for finding alternative material parameters for 2-D transformation electromagnetics (inhomogeneous, anisotropic) devices [55]. The alternative material parameters support exactly the same field pattern as the original ones of the transformation electromagnetics device. The same method was also extended to design dual functional transformation electromagnetics devices that combine the characteristics of two separate transformation devices into one. An analytical formulation was shown in [55] and the results were verified through the full-wave simulation of well-known transformation electromagnetics devices: an electromagnetic field rotator and a cylindrical electromagnetic field concentrator. Although the transformation electromagnetics devices possessing alternative material parameters only work for a particular illumination direction, the method presented will find application in the design of antennas and beam-forming networks with a fixed feed position.

4. *A Transformation-Designed Device Implemented with Tensor Transmission-Line Metamaterials*

To demonstrate the utility of tensor transmission-line metamaterials in implementing devices with anisotropic and inhomogeneous material parameters, a planar transformation electromagnetics device was implemented [56]. A beam-shifting slab (a transformation electromagnetics device) was implemented using tensor transmission-line metamaterials. A photograph of the device is shown in Fig. 9. A beam-shifting slab is an anisotropic, homogeneous and reflectionless slab which laterally displaces the electromagnetic field transmitted through it. The experimental beam-shifting slab consists of printed tensor transmission-line unit cells exhibiting anisotropic effective material parameters, while the surrounding medium consists of printed isotropic unit cells. The measured and simulated field patterns within the beam-shifting slab and the surrounding media were compared and showed excellent agreement. Simulation and experimental results demonstrated that radiation from a cylindrical source is shifted upward by 5.28 unit cells due to the presence of the beam-shifting slab. Furthermore, the wide-band frequency response of the slab was experimentally studied.

The reported results experimentally verified the theory behind tensor transmission-line metamaterials and demonstrated their utility in the design of transformation electromagnetics devices at microwave frequencies. They showed how tensor TL metamaterials have enabled the design and implementation of transformation electromagnetics devices using circuit networks.

5. *Tailoring the Phase and Power Flow of Electromagnetic Fields with Metamaterials*

The formulation for finding alternative material parameters for transformation electromagnetics devices motivated further work. It led to the development of a method for arbitrarily controlling the phase progression and power flow of electromagnetic fields within a 2D region of space [57]. The formulation describes how a 2D inhomogeneous, anisotropic medium can be designed that supports desired spatial distributions of the wave vector and Poynting vector direction. Plane-wave relations in anisotropic media were used in conjunc-

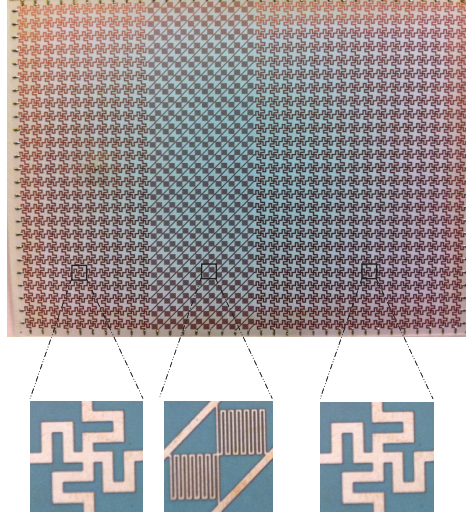


FIG. 9. The experimental structure showing the printed beamshifting slab (consisting of anisotropic unit cells) surrounded by a medium (consisting of isotropic unit cells). The structure was fabricated using standard printed circuit board fabrication processes. The corresponding anisotropic (center) and isotropic unit cells (on each side) are shown in the inset.

tion with an impedance matching process to find the required material parameters. The proposed design approach provides independent spatial control of phase progression and power flow. Such control allows one to independently tailor the phase and amplitude of a field profile. It could find use in the design of a wide range of electromagnetic devices including antennas and beam-forming networks, and may also find application in scattering control and holography. Figure 10 shows a 2D inhomogeneous, anisotropic region that was designed using the proposed approach. It converts an incident cylindrical wave at boundary 1 to a field profile with a triangular power density distribution and uniform phase at boundary 2.

C. Impact

The proposed design approach provides independent spatial control of the phase progression and power flow of electromagnetic waves within a 2D medium. This control can be extended to surfaces through the use of tensor transmission-line metamaterials. The design approach will find use in the development of a wide range of electromagnetic devices including antennas and beam-forming networks, and may also find application in scattering control [58, 59] and holography [60, 61]. It could provide a novel approach to signal routing, the design of mode conversion devices [62], and the generation of extreme antenna apertures for super-directive radiation [63] or the excitation of Airy [64–67] and Bessel beams [68–71]. For example, in antenna design, one may wish to control power flow across an aperture in order to realize a given amplitude distribution (beam shape), while at the same time control phase progression to establish a certain beam-pointing direction. In the case of a beam-former, one may wish to stipulate an input field distribution (excitation) and an output field distribution (amplitude and phase distribution of the antenna elements), with a transition from one to the other. Therefore, spatial control of phase and power flow also

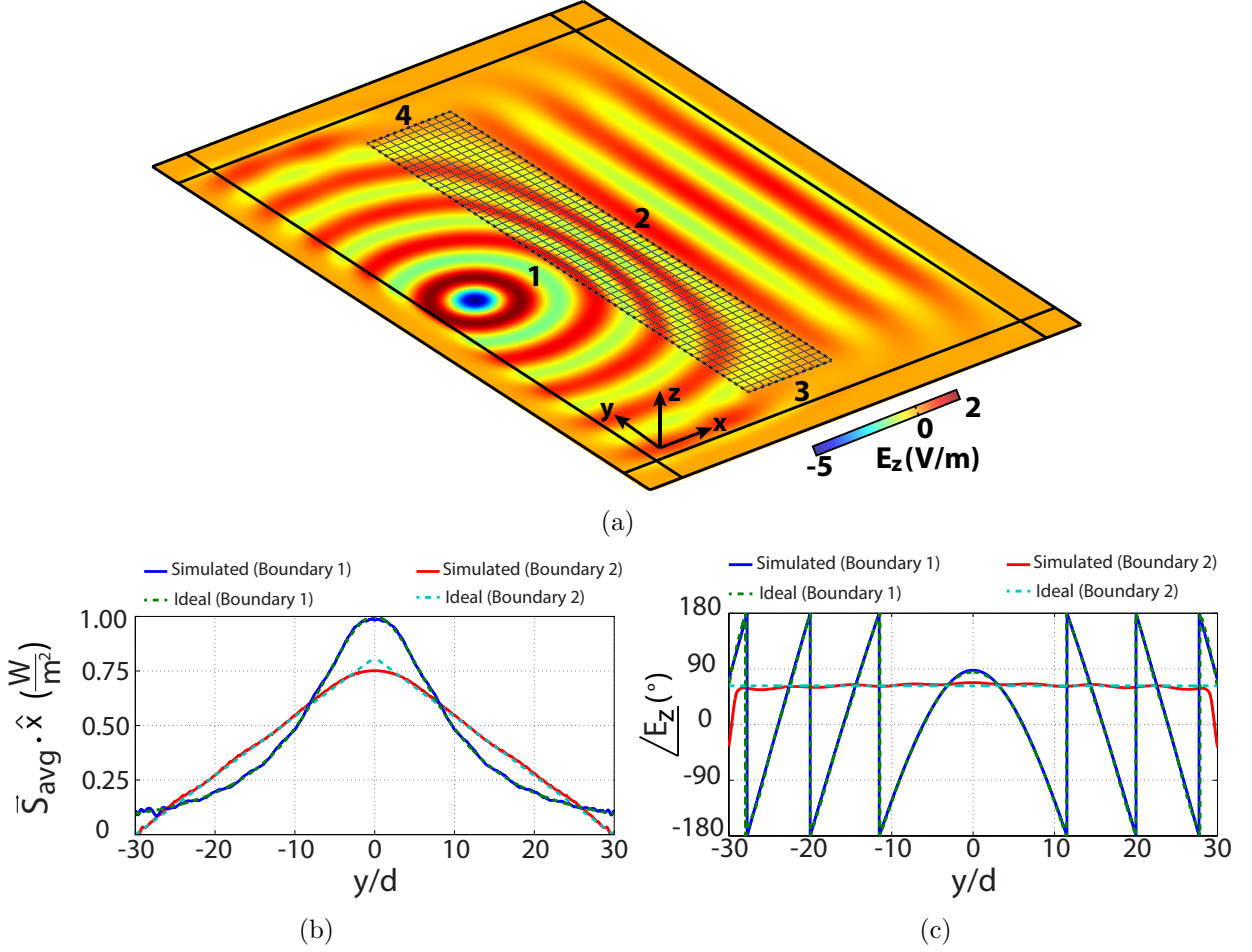


FIG. 10. (color online). (a) Time snapshot of the simulated, vertical electric field (E_z) within an surrounding the designed 2D inhomogeneous, anisotropic region. (b) Simulated and ideal power densities along boundary 1 and boundary 2. (c) Phase profiles along boundary 1 and boundary 2.

allows one to independently mold the phase and amplitude of a field profile.

Earlier works have attempted to control these two quantities through coordinate transformations. Finite embedded coordinate transformation method introduced in [72] was used to laterally displace the power flow of an Gaussian beam while preserving its phase progression. On the other hand, [73] showed how to control the phase-front of a beam while retaining its power flow direction. Here, we demonstrate simultaneous control over both the phase progression and power flow of electromagnetic fields without defining a coordinate transformation.

IV. PERSONNEL SUPPORTED

The following people were supported by this research effort:

- PI: Anthony Grbic.
- Graduate Students: Scott Rudolph, Mohammadreza F. Imani, Amit Patel, Gurkan Gok, Carl Pfeiffer, Lai Wei, Brian Tierney, Adam Weiss, and Nikolaos Chiotellis.

- Postdoctoral Researcher: Francis Elek.
- Visiting Scholar: Mauro Ettorre.
- Summer Undergraduate Researchers: Tony Chen, Brett Kuprel, and Dike Zhou.

V. PUBLICATIONS

Publications stemming from this research effort are listed below.

A. Journal Papers

1. J. D. Heebl and A. Grbic, "Comprehensive analysis and measurement of frequency-tuned and impedance-tuned wireless non-radiative power transfer systems," *IEEE Antennas and Propagation Magazine*, accepted, to appear in October 2014.
2. B. B. Tierney, A. Grbic, "Planar shielded-loop resonators," *IEEE Trans. on Antennas and Propagation*, vol.62, no.6, pp.3310-3320, June 2014.
3. A. M. Patel and A. Grbic, "Transformation electromagnetics devices based on printed-circuit tensor impedance surfaces," *IEEE Trans. on Microwave Theory and Techniques*, vol. 62, pp. 1102 - 1111, May 2014.
4. B. B. Tierney and A. Grbic. "Design of self-matched planar loop resonators for wireless nonradiative power transfer." *IEEE Trans. on Microwave Theory Techniques*, 62 pp. 909-919, April 2014.
5. A. M. Patel and A. Grbic, "The effects of spatial dispersion on power flow along a printed-circuit tensor impedance surface," *IEEE Trans. on Antennas and Propagation*, vol. 62, no. 3, pp. 1464-1469, March 2014.
6. M. F. Imani and A. Grbic. "A unidirectional subwavelength focusing near-field plate," *Journal of Applied Physics*, vol. 115, no. 4, 044904, January 2014.
7. M. F. Imani and A. Grbic, "Planar near-field plates," *IEEE Trans. on Antennas and Propagation*, vol. 61, no. 11, pp. 5425-5434, November 2013.
8. E. Gandini, M. Ettorre, R. Sauleau, A. Grbic, "A lumped-element unit cell for beam-forming networks and its application to a miniaturized butler matrix" *IEEE Trans. on Microwave Theory and Techniques*, vol. 61, pp. 1477-1487, April 2013.
9. A. M. Patel and A. Grbic, "Effective surface impedance of a printed-circuit tensor impedance surface (PCTIS)" *IEEE Trans. on Microwave Theory and Techniques*, vol. 6, pp. 1403-1413, April 2013.
10. G. Gok and A. Grbic, "Alternative material parameters for transformation electromagnetics designs," *IEEE Trans. on Microwave Theory and Techniques*, vol. 61, pp. 1414-1424, April 2013.
11. G. Gok and A. Grbic "A printed beam-shifting slab designed using tensor transmission-line metamaterials," *IEEE Trans on Antennas and Propagation*, vol. 61, pp. 728-734, Feb. 2013.
12. A. M. Patel, A. Grbic, "Modeling and analysis of printed-circuit tensor impedance surfaces," *IEEE Trans. on Antennas and Propagation*, vol. 61, pp.211-220, January 2013

13. E. M. Thomas, J.D. Heeb, C. Pfeiffer, A. Grbic, "A power link study of wireless non-radiative power transfer systems using resonant shielded loops," *IEEE Trans. on Circuits and Systems I*, vol. 59, pp. 2125-2136, September 2012.
14. S. M. Rudolph and A. Grbic, "A broadband three-dimensionally isotropic negative-refractive-index medium," *IEEE Trans. on Antennas and Propagation*, vol. 60, pp. 3661 - 3669, August 2012.
15. M. Ettorre and A. Grbic, "Generation of propagating bessel beams using leaky-wave modes," *IEEE Trans. on Antennas and Propagation*, vol. 60, pp. 3605 - 3613 August 2012
16. M. F. Imani and A. Grbic, "Generating evanescent bessel beams using near-field plates," *IEEE Trans. on Antennas and Propagation*, vol. 60, pp. 3155-3164, July 2012.
17. M. Ettorre and A. Grbic, "Generation of propagating bessel beams using leaky-wave modes: experimental validation," *IEEE Trans. on Antennas and Propagation*, vol. 60, pp. 2645 - 2653 June 2012.
C. Pfeiffer and A. Grbic, "A circuit model for electrically small antennas," *IEEE Trans. on Antennas and Propagation*, vol. 60, pp. 1671-1683, April 2012.
18. C. Pfeiffer, X. Xu, S. R. Forrest, and A. Grbic, "Direct transfer patterning of electrically small antennas onto three dimensionally contoured substrates," *Advanced Materials*, vol. 24, pp. 1166-1170, March 2012.
19. G. Gok and A. Grbic, "Homogenization of tensor TL metamaterials," *Metamaterials*, vol. 5, pp. 81-89, June-Sept 2011. (invited to the *Metamaterials 2010 Congress Special issue*)
20. S.M. Rudolph and A. Grbic, "Design and free-space measurements of broadband, low-loss negative-permeability and negative-index media," *IEEE. Trans. on Antennas and Propagation*, vol. 59, pp. 2989-2997, August 2011.
21. A. M. Patel and A. Grbic, "A printed leaky-wave antenna based on a sinusoidally-modulated reactance surface," *IEEE Transactions on Antennas and Propagation*, vol. 59, pp. 2087-2096, April 2011.
22. A. Grbic, R. Merlin, E.M. Thomas, M.F. Imani, "Near-field plates: metamaterial surfaces / arrays for subwavelength focusing and probing," *Proceedings of the IEEE*, vol. 99, pp. 1806-1815, October 2011. (invited to the special issue on *Metamaterials: Fundamentals and Applications in the Microwave and Optical Regimes*).
23. M.F. Imani and A. Grbic, "An experimental concentric near-field plate," *IEEE Transactions on Microwave Theory and Techniques*, vol. 58, no. 12, pp. 3982 - 3988, December 2010.
24. M. F. Imani and A. Grbic, "An analytical investigation of near-field plates," *Metamaterials*, vol. 4, pp. 104-111, August-September 2010 (invited to the *Metamaterials 2009 Congress Special issue*).
25. C. Pfeiffer and A. Grbic, "A printed, broadband Luneburg lens antenna," *IEEE Transactions on Antennas and Propagation*, vol. 58, no. 9, pp. 3055 - 3059 September 2010.
26. G. Gok and A. Grbic, "Tensor transmission-line metamaterials," *IEEE Transactions on Antennas and Propagation*, vol. 58, no. 5, pp. 1559 - 1566, May 2010.

B. Letters

1. G. Gok, A. Grbic. "Tailoring the phase and power flow of electromagnetic fields." *Physical Review Letters* 111, no. 23, 33904, December 2013.

2. S. M. Young, C. Pfeiffer, A. Grbic, and R. Merlin, "Enhanced resonant transmission of electromagnetic radiation through a pair of subwavelength slits," *Applied Physics Letters*, vol. 103, 041104, July 2013.
3. C. Pfeiffer and A. Grbic, "Cascaded metasurfaces for complete phase and polarization control," *Applied Physics Letters*, 102, 231116, June 2013.
4. C. Pfeiffer and A. Grbic, "Metamaterial huygens' surfaces: tailoring wavefronts with reflectionless sheets," *Physical Review Letters*, vol. 110, 197401, May 2013.
5. M. Ettore and A. Grbic, "Transponder-based, non-radiative wireless power transfer," *IEEE Antennas and Wireless Propagation Letters*, vol.11, pp.1150-1153, 2012.
6. B. Kuprel and A. Grbic, "Anisotropic, inhomogeneous metamaterials using non-uniform transmission-line grids aligned with the principal axes," *IEEE Antennas and Wireless Propagation Letters*, vol. 11, pp. 358-361, April 2012.
7. G. Gok and A. Grbic, "Full-Wave verification of tensor transmission-line metamaterials," *IEEE Antennas and Wireless Propagation Letters*, vol. 9, pp. 48 - 51, February 2010.
8. M. F. Imani and A. Grbic, "Tailoring near-field patterns with concentrically corrugated plates," *Applied Physics Letters*, vol. 95, pp. 111107, September 2009.
9. M. F. Imani and A. Grbic, "Near-field focusing with a corrugated surface," *IEEE Antennas and Wireless Propagation Letters*, vol. 8, pp. 421 - 424, May 2009.
10. T. Andrade, A. Grbic and G.V. Eleftheriades, "Growing evanescent waves in continuous transmission-line grid media," *IEEE Microwave and Wireless Components Letters*, vol. 15, no. 2, pp. 131-133, February 2005.
11. A. Grbic and G.V. Eleftheriades, "Overcoming the diffraction limit with a planar left-handed transmission-line lens," *Physical Review Letters*, vol. 92, no. 11, 117403, March 19, 2004 (front cover of the March issue).
12. A. Grbic and G.V. Eleftheriades, "Sub-wavelength focusing using a negative-refractive-index transmission-line lens," *IEEE Antennas and Wireless Propagation Letters*, vol. 2, pp. 186-189, 2003.
13. A. Grbic and G.V. Eleftheriades, "Dispersion analysis of a microstrip based negative refractive index periodic structure," *IEEE Microwave and Wireless Components Letters*, vol. 13, no. 4, pp. 155-157, April 2003.
14. A. Grbic and G.V. Eleftheriades, "Growing evanescent waves in negative-refractive-index transmission-line media," *Applied Physics Letters*, vol. 82, no. 12, pp. 1815-1817, March 24, 2003.

C. Conference Papers

1. M. Ettore, G. Valerio, R. Sauleau, W. Fuscaldo, A. Galli, A. Grbic, "Generation of non-diffractive Bessel beams using leaky-wave modes," *The European Microwave Conference*, pp. 1-5, Rome, Italy, October 5-10, 2014 (invited).
2. B. B. Tierney and A. Grbic, "Far-field synthesis using impedance surfaces supporting leaky waves," *International Congress on Advanced Electromagnetic Materials in Microwaves and Optics (Metamaterials 2014)*, pp. 1-3, Copenhagen, Denmark, Aug 25-30, 2014 (invited).

3. B. B. Tierney and A. Grbic, "Tailoring Leaky-Wave Radiation with Impedance Surfaces," URSI General Assembly and Scientific and Scientific Symposium, pp. 1-4, Beijing, China, August 16-23, 2014 (invited).
4. F. Elek and A. Grbic, "Phase and power flow along printed-circuit tensor impedance surfaces," IEEE International Symposium on Antennas and Propagation, pp. 1-2, Memphis, TN, July 6-12, 2014.
5. Pfeiffer and A. Grbic, "Analysis and synthesis of bianisotropic metasurfaces," IEEE International Symposium on Antennas and Propagation, pp. 1-2, Memphis, TN, July 6-12, 2014.
6. B. B. Tierney and A. Grbic, "Tailoring leaky-wave radiation with impedance surfaces," IEEE International Symposium on Antennas and Propagation, pp. 1-2, Memphis, TN, July 6-12, 2014.
7. A. Grbic and G. Gok, "A printed antenna beam former implemented using tensor transmission-line metamaterials," IEEE International Symposium on Antennas and Propagation, pp. 1-2, Memphis, TN, July 6-12, 2014.
8. A. Weiss and A. Grbic, "Backward wave amplifier based on an NRI transmission-line metamaterial," IEEE International Symposium on Antennas and Propagation, pp. 1-2, Memphis, TN, July 6-12, 2014.
9. C. Pfeiffer, N. K. Emani, A. M. Shaltout, A. Boltasseva, V. M. Shalaev and A. Grbic, "Experimental Huygens' Surface for NIR Wavelengths," CLEO: QELS Fundamental Science, pp. 1-3, San Jose, California, June 8-13, 2014.
10. G. Gok and A. Grbic, "Controlling phase and power flow with electromagnetic metamaterials," International Conference on Metamaterials, Photonic Crystals and Plasmonics, Singapore, May 20-23, 2014 (invited).
11. C. Pfeiffer and A. Grbic, "A refracting metasurface that converts linear to circular polarization," International Conference on Metamaterials, Photonic Crystals and Plasmonics, Singapore, May 20-23, 2014 (invited).
12. A. Grbic and G. Gok, "Generating field profiles with arbitrary phase and amplitude distributions using metamaterials," European Conference on Antennas and Propagation, The Hague, The Netherlands, April 6-11, 2014 (invited).
13. C. Pfeiffer and A. Grbic, "Metamaterial Huygens' surfaces from microwave to optical frequencies", European Conference on Antennas and Propagation, pp. 1-3, The Hague, The Netherlands, April 6-11, 2014 (invited).
14. C. Pfeiffer and A. Grbic, "Manipulating wavefronts with metamaterial huygens' surfaces," International Congress on Advanced Electromagnetic Materials in Microwaves and Optics (Metamaterials 2013), Bordeaux, France, Sept 16-19, 2013 (invited).
15. B. B. Tierney and A. Grbic, "Planar shielded-loop resonators for wireless non-radiative power transfer," IEEE International Symposium on Antennas and Propagation, pp. 1-2, Orlando, FL, July 7-13, 2013.
16. G. Gok and A. Grbic, "Controlling the phase and power flow of electromagnetic fields," IEEE International Symposium on Antennas and Propagation, pp. 1-2, Orlando, FL, July 7-13, 2013.
17. M. F. Imani and A. Grbic, "Generating bessel beams using an electrically-large annular slot," IEEE International Symposium on Antennas and Propagation, pp. 1-2, Orlando, FL, July 7-13, 2013.

18. M. Ettorre, M. Casaletti, and A. Grbic, "Power Link budget for propagating bessel beams," IEEE International Symposium on Antennas and Propagation, pp. 1-2, Orlando, FL, July 7-13, 2013.
19. L. Gomez, L. Hernandez-Garcia, A. Grbic, E. Michielssen, "Single-source multi-coil transcranial magnetic stimulators for deep and focused stimulation of the human brain," IEEE International Symposium on Antennas and Propagation, pp. 1-2, Orlando, FL, July 7-13, 2013.
20. C. Pfeiffer and A. Grbic, "Metamaterial huygens' surfaces," IEEE MTT-S International Microwave Symposium, 3 pages, Seattle, WA, June 2-7 2013.
21. A.M. Patel and A. Grbic, "Transformation electromagnetics devices based on printed-circuit tensor impedance surfaces," IEEE MTT-S International Microwave Symposium, 3 pages, Seattle, WA, June 2-7 2013.
22. A. Grbic, G. Gok, M.F. Imani, A.M. Patel, C. Pfeiffer, and M. Ettorre, "Metamaterial surfaces for near and far-field applications," European Conference on Antennas and Propagation, pp. 3618 - 3622, Gothenburg, Sweden, April 8-12, 2013 (invited).
23. G. Gok and A. Grbic, "Alternative material parameters for transformation optics designs" International Conference on Advanced Electromagnetic Materials in Microwaves and Optics (Metamaterials 2012), 3 pages, St. Petersburg, Russia, Sept. 17-22, 2012 (invited).
24. C. Pfeiffer and A. Grbic, "Realizing huygens sources through spherical sheet impedances", IEEE International Symposium on Antennas and Propagation, pp. 1-2, Chicago IL, July 8-14, 2012.
25. A. M. Patel and A. Grbic, "Dispersion analysis of printed-circuit tensor impedance surfaces", IEEE International Symposium on Antennas and Propagation, pp. 1-2, Chicago IL, July 8-14, 2012.
26. M. Ettorre, S.M. Rudolph and A. Grbic, "A Leaky-radial waveguide for generating propagating bessel beams", IEEE International Symposium on Antennas and Propagation, pp. 1-2, Chicago IL, July 8-14, 2012.
27. E. Gandini, M. Ettorre, R. Sauleau, and A. Grbic, "Compact directional coupler and its application as building block for beam-forming networks", IEEE International Symposium on Antennas and Propagation, pp. 1-2, Chicago IL, July 8-14, 2012.
28. M. F. Imani and A. Grbic, "Design of a planar near-field plate", IEEE International Symposium on Antennas and Propagation, pp. 1-2, Chicago IL, July 8-14, 2012.
29. G. Gok and A. Grbic, "A beam-shifting slab implemented using printed, tensor TL metamaterials," IEEE MTT-S International Microwave Symposium, 4 pages, Montreal Canada, June 17-22 2012.
30. A. M. Patel and A. Grbic, "Analytical modeling of a printed-circuit tensor impedance surface," IEEE MTT-S International Microwave Symposium, 4 pages, Montreal Canada, June 17-22 2012.
31. E. Gandini, M. Ettorre, R. Sauleau, A. Grbic, "A lumped-element directional coupler with arbitrary output amplitude and phase distributions," IEEE MTT-S International Microwave Symposium, 4 pages, Montreal Canada, June 17-22 2012.
32. M. Ettorre and A. Grbic, "Experimental generation of propagating bessel beams with a low-profile leaky radial waveguide," European Conference on Antennas and Propagation (EuCAP), pp. 1-4, March 26-30, 2012.
33. E. Gandini, M. Ettorre, R. Sauleau, and A. Grbic, "Lumped-element unit cell for designing beam-forming networks," European Conference on Antennas and Propagation (EuCAP), pp. 1-4, March 26-30, 2012.

34. G. Gok and A. Grbic, "Tensor circuit networks for transformation optics," International Conference on Advanced Electromagnetic Materials in Microwaves and Optics (Metamaterials 2010), 3 pages, Barcelona Spain, Oct. 10-14 2011 (invited).
35. C. Pfeiffer, X. Xu, S.R. Forrest, A. Grbic, "Novel methods to analyze and fabricate electrically small antennas, IEEE International Symposium on Antennas and Propagation, pp. 761-764, Spokane WA, July 3-8, 2011 (student paper contest finalist).
36. C. Pfeiffer and A. Grbic, "Equivalent circuits for electrically small antennas," European Conference on Antennas and Propagation (EuCAP), pp. 2666-2668, April 11-15, 2011 (invited).
37. G. Gok and A. Grbic, "Tensor transmission-line metamaterials and their applications, European Conference on Antennas and Propagation (EuCAP), pp. 3313-3315, April 11-15, 2011 (invited).
38. S.M. Rudolph and A. Grbic, "The design and performance of an isotropic negative-refractive-index metamaterial lens," URSI General Assembly and Scientific Symposium, pp. 1-4, Istanbul, Turkey, Aug. 13-20, 2011.
39. A. Grbic, G. Gok and S. M. Rudolph, "Advances in planar and volumetric metamaterials," 20th International Conference on Applied Electromagnetics and Communications (ICECOM), 4 pages, Dubrovnik, Croatia, Sept. 20-23, 2010 (invited).
40. A. Grbic and G. Gok, "Tensor metamaterials based on transmission-line networks," 4th International Conference on Advanced Electromagnetic Materials in Microwaves and Optics (Metamaterials 2010), 3 pages, Karlsruhe, Germany, Sept. 13-16 2010 (invited).
41. C. Pfeiffer, X. Xu, S. R. Forrest and A. Grbic, "A printed spherical helix antenna," 14th International Symposium on Antenna Technology and Applied Electromagnetics (ANTEM), 4 pages, Ottawa, Canada, July 5-9, 2010.
42. E. M. Thomas, J. D. Heebl, A. Grbic, "Shielded loops for wireless non-radiative power transfer," IEEE International Symposium on Antennas and Propagation, 4 pages, Toronto, Canada, July 11-17 2010.
43. S. M. Rudolph and A. Grbic, "A broadband three-dimensional isotropic NRI medium," IEEE International Symposium on Antennas and Propagation, 4 pages, Toronto, Canada, July 11-17 2010, (invited).
44. M. F. Imani and A. Grbic, "A concentrically corrugated near-field plate," IEEE MTT-S International Microwave Symposium, 4 pages, Anaheim, CA, May 23-28 2010.
45. A. Grbic and G. Gok, "Transformation circuits," European Conference on Antennas and Propagation (EuCAP), 3 pages, Barcelona, Spain, April 12-16 2010 (invited).
46. M. F. Imani and A. Grbic, "Design and implementation of near-field plates," 3rd International Conference on Advanced Electromagnetic Materials in Microwaves and Optics (Metamaterials 2009), 3 pages, London, England, August 30 - September 4 2009 (invited).
47. S. M. Rudolph and A. Grbic, "Broadband, low-loss negative permeability and negative-index media for free-space applications," IEEE MTT-S International Microwave Symposium, pp. 113-116, Boston MA, June 15-20 2009.
48. M. F. Imani and A. Grbic, "Subwavelength focusing with a corrugated metallic plate," IEEE International Symposium on Antennas and Propagation, 4 pages, Charleston SC, June 1-5 2009.

49. A. M. Patel and A. Grbic, "A printed leaky-wave antenna with a sinusoidally-modulated surface reactance," IEEE International Symposium on Antennas and Propagation, 4 pages, Charleston SC, June 1-5 2009.
50. C. Pfeiffer and A. Grbic, "A 2D broadband, printed Luneburg Lens Antenna," IEEE International Symposium on Antennas and Propagation, 4 pages, Charleston SC, June 1-5 2009.

-
- [1] D. R. Smith R. A. Shelby and S. Schultz, “Experimental verification of a negative index of refraction,” *Science* **292**, 77–79 (2001).
 - [2] J. B. Pendry, “Negative refraction makes a perfect lens,” *Physical Review Letters* **85**, 3966–3969 (2000).
 - [3] J. B. Pendry and D.R. Smith, “The quest for the superlens,” *Scientific American* , 60–67 (2006).
 - [4] A. Grbic and G. V. Eleftheriades, “Overcoming the diffraction limit with a planar left-handed transmission-line lens,” *Physical Review Letters* **92**, 117403 (2004).
 - [5] J. B. Pendry M. C. K Wiltshire and J. V. Hajnal, “Sub-wavelength imaging at radio frequency,” *Journal of Physics: Condensed Matter* **18**, L315–L321 (2006).
 - [6] C. Sun N. Fang, H. Lee and X. Zhang, “Sub-diffraction-limited optical imaging with a silver superlens,” *Science* **308**, 534–537 (2005).
 - [7] D. Melville and R. Blaikie, “Super-resolution imaging through a planar silver layer,” *Optics Express* **13**, 2127–2134 (2005).
 - [8] R. Marques F. Mesa, M. J. Freire and J. D. Baena, “Three dimensional superresolution in metamaterial slab lenses: experiment and theory,” *Physical Review B* **72**, 235117 (2005).
 - [9] R. Merlin, “Radiationless electromagnetic interference: evanescent-field lenses and perfect focusing,” *Science* **317**, 927–929 (2007).
 - [10] A. Grbic and R. Merlin, “Near-field focusing plates and their design,” *IEEE Trans. on Antennas and Propagation* **56**, 3159–3165 (2008).
 - [11] A. Grbic, L. Jiang and R. Merlin, “Near-field plates: subdiffraction focusing with patterned surfaces,” *Science* **320**, 511–513 (2008).
 - [12] M. F. Imani and A. Grbic, “Subwavelength focusing with a corrugated metallic plate,” in *IEEE International Symposium on Antennas and Propagation* (Charleston, SC, 2009).
 - [13] M. F. Imani and A. Grbic, “Near-field focusing with a corrugated surface,” *IEEE Antennas and Wireless Propagation Letters* **8**, 421–424 (2009).
 - [14] M. F. Imani and A. Grbic, “Tailoring near-field patterns with concentrically corrugated plates,” *Applied Physics Letters* **95**, 111107 (2009).
 - [15] M. F. Imani and A. Grbic, “A concentrically corrugated near-field plate,” in *IEEE MTT-S International Microwave Symposium* (Anaheim, CA, 2010) pp. 1648–1651.
 - [16] M. F. Imani and A. Grbic, “An analytical investigation of near-field plates,” *Metamaterials* **4**, 104–111 (2009).
 - [17] G. V. Eleftheriades and A. M. H. Wong, “Holography-inspired screens for sub-wavelength focusing in the near field,” *IEEE Microwave and Wireless Component Letters* **18**, 236–238 (2008).
 - [18] L. Markley and G. V. Eleftheriades, “Two dimensional subwavelength focusing using a slotted meta-screen,” *IEEE Microwave and Wireless Components Letters* **19**, 137–139 (2009).
 - [19] L. Markley, A. M. H. Wong, Y. Wang and G. V. Eleftheriades, “Spatially shifted beam approach to subwavelength focusing,” *Physical Review Letters* **101**, 113901 (2008).
 - [20] E. F. Kuester, M. A. Mohamed, M. Piket-May and C. L. Holloway, “Averaged Transition Conditions for Electromagnetic Fields at a Metafilm,” *IEEE Trans. on Antennas and Propagation* **51**, 2641–2651 (2003).

- [21] M. F. Imani and A. Grbic, "An experimental concentric near-field plate," *IEEE Trans. on Microwave Theory and Techniques* **58**, 3982–3988 (2010).
- [22] L. Markley and G. V. Eleftheriades, "A near-field probe for subwavelength-focused imaging," *IEEE Trans. on Microwave Theory and Techniques* **58**, 551–558 (2010).
- [23] L. Markley and G. V. Eleftheriades, "Two-dimensional subwavelength-focused imaging using a near-field probe at a $\lambda/4$ working distance," *Journal of Applied Physics* **107**, 093102 (2010).
- [24] E.M. Thomas M. F. Imani A. Grbic, R. Merlin, "Near-field plates: Metamaterial surfaces/arrays for subwavelength focusing and probing," *Proceedings of the IEEE* **99**, 1806–1815 (2011).
- [25] L. Novotny and B. Hecht, *Principles of nano-optics* (Cambridge Press, 2006) p. 196.
- [26] V. V. Talanov S. M. Anlage and A. R. Schwartz, "Principles of near-field microwave microscopy," in *Scanning Probe Microscopy: Electrical and Electromechanical Phenomena at the Nanoscale*, edited by S. V. Kalinin and A. Gruverman (Springer-Verlag, New York, 2007) Chap. I.7, pp. 215–253.
- [27] Seyedmohammadreza Faghih Imani, *Theory and Development of Near-field Plates*, Ph.D. thesis, University of Michigan, Ann Arbor (2013).
- [28] Mohammadreza F Imani and Anthony Grbic, "Generating evanescent bessel beams using near-field plates," *IEEE Trans. on Antennas and Propagation* **60**, 3155–3164 (2012).
- [29] M.F. Imani and A. Grbic, "Planar near-field plates," *IEEE Trans. on Antennas and Propagation* **61**, 5425–5434 (2013).
- [30] Mohammadreza F Imani and Anthony Grbic, "A unidirectional subwavelength focusing near-field plate," *Journal of Applied Physics* **115**, 044904 (2014).
- [31] Mohammadreza F Imani and Anthony Grbic, "Unidirectional wireless power transfer using near-field plates," *Journal of Applied Physics*, submitted (2014).
- [32] R.P. Penno J. D. Heebl, E.M. Thomas and A. Grbic, "Comprehensive analysis and measurement of frequency-tuned and impedance-tuned wireless non-radiative power-transfer systems," *IEEE Antennas and Propagation Magazine* **56**, 40–66 (2014).
- [33] J. D. Joannopoulos A. Karalis and M. Soljacic, "Efficient wireless non-radiative mid-range energy transfer," *Annals of Physics* **323**, 34–48 (2008).
- [34] S. Lee L. Hernandez-Garcia and W. Grissom, "An approach to MRI-based dosimetry for transcranial magnetic stimulation," *NeuroImage* **36**, 1171–1178 (2007).
- [35] I. Tsukerman, "Superfocusing by nanoshells," *Optics Letters* **34**, 1057–1059 (2009).
- [36] R. Gordon, "Proposal for superfocusing at visible wavelengths using radiationless interference of a Plasmonic Array," *Physical Review Letters* **102**, 207402 (2009).
- [37] Y. Wang, A. M. H. Wong, L. Markley, A. S. Helmy and G. V. Eleftheriades, "Plasmonic meta-screen for alleviating the trade-offs in the near-field optics," *Optics Express* **17**, 12351–12361 (2009).
- [38] L. Scoranno, F. Bilotti and L. Vegni, "Design of a meta-screen for near-zone field focalizatoin at optical frequencies," *Microwave and Optical Technology Letters* **51**, 2718–2721 (2009).
- [39] H. Shi and J. Guo, "Design of plasmonic near field plate at optical frequency," *Applied Physics Letters* **96**, 141107 (2010).
- [40] A. Rashidi and H. Mosallaei, "Array of Plasmonic particles enabling optical near-field concentration: a nonlinear inverse scattering approach," *Physical Review B* **82**, 035117 (2010).
- [41] A. Salandrino N. Engheta and A. Alu, "Circuit elements at optical frequencies: nanoinductors, nanocapacitors, and nanoresistors," *Physical Review Letters* **95**, 095504 (2005).

- [42] L. E. Helseth, "Focusing of evanescent vector waves," *Optics Communications* **283**, 29–33 (2010).
- [43] John B Pendry, David Schurig, and David R Smith, "Controlling electromagnetic fields," *Science* **312**, 1780–1782 (2006).
- [44] Gurkan Gok, *Tensor Transmission-Line Metamaterials*, Ph.D. thesis, University of Michigan, Ann Arbor (2014).
- [45] G. Gok and A. Grbic, "Tensor transmission-line metamaterials," *IEEE Trans. on Antennas and Propagation* **58**, 1559–1566 (2010).
- [46] G.V. Eleftheriades, A.K. Iyer, and P.C. Kremer, "Planar negative refractive index media using periodically L-C loaded transmission lines," *IEEE Trans. on Microwave Theory and Techniques* **50**, 2702–2712 (2002).
- [47] A. Grbic and G.V. Eleftheriades, "Periodic analysis of a 2-D negative refractive index transmission line structure," *IEEE Trans. on Antennas and Propagation* **51**, 2604–2611 (2003).
- [48] A. Grbic and G.V. Eleftheriades, "Negative refraction, growing evanescent waves, and sub-diffraction imaging in loaded transmission-line metamaterials," *IEEE Trans. on Microwave Theory and Techniques* **51**, 2297–2305 (2003).
- [49] G.V. Eleftheriades and O.F. Siddiqui, "Negative refraction and focusing in hyperbolic transmission-line periodic grids," *IEEE Trans. on Microwave Theory and Techniques* **53**, 396–403 (2005).
- [50] K.G. Balmain, A.A.E. Luttgen, and P.C. Kremer, "Power flow for resonance cone phenomena in planar anisotropic metamaterials," *IEEE Trans. on Antennas and Propagation* **51**, 2612–2618 (2003).
- [51] J.K.H. Wong, K.G. Balmain, and G.V. Eleftheriades, "Fields in planar anisotropic transmission-line metamaterials," *IEEE Trans. on Antennas and Propagation* **54**, 2742–2749 (2006).
- [52] C. Caloz and T. Itoh, "Positive/negative refractive index anisotropic 2-D metamaterials," *IEEE Microwave and Wireless Components Letters* **13**, 547–549 (2003).
- [53] C. Caloz, C.-H. Ahn, and T. Itoh, "Analysis 2D finite-size metamaterials by the transmission matrix method," in *IEEE Antennas and Propagation Society International Symposium*, Vol. 3B (Washington, DC, 2005) pp. 2–5.
- [54] G. Gok and A. Grbic, "Full-wave verification of tensor tl metamaterials," *IEEE Antennas and Wireless Propagation Letters* **9**, 48–51 (2010).
- [55] G. Gok and A. Grbic, "Alternative material parameters for transformation electromagnetics designs," *IEEE Trans. on Microwave Theory and Techniques* **61**, 1414–1424 (2013).
- [56] G. Gok and A. Grbic, "A printed beam-shifting slab designed using tensor transmission-line metamaterials," *IEEE Trans. on Antennas and Propagation* **61**, 728–734 (2013).
- [57] G. Gok and A. Grbic, "Tailoring the phase and power flow of electromagnetic fields," *Physical Review Letters* **111**, 233904 (2013).
- [58] D. Sievenpiper, J. Colburn, B. Fong, J. Ottusch, and J. Visher, "Holographic artificial impedance surfaces for conformal antennas," in *Proceedings of IEEE Antennas and Propagation Society International Symposium (APSURSI)* (Washington, DC, 2005) pp. 256–259.
- [59] B. H. Fong, J. S. Colburn, J. J. Ottusch, J. L. Visher, and D. F. Sievenpiper, "Scalar and tensor holographic artificial impedance surfaces," *IEEE Trans. on Antennas and Propagation* **58**, 3212–3221 (2010).
- [60] P. Hariharan, *Optical Holography: Principles, Techniques and Applications* (Cambridge Univ. Press, 1996) pp. 11–13.

- [61] P. Checcacci, V. Russo, and A. Scheggi, “Holographic Antennas,” *IEEE Trans. on Antennas and Propagation* **18**, 811–813 (1970).
- [62] M. Yang, J. Li, and K. J. Webb, “Functional waveguide mode transformers,” *IEEE Trans. on Microwave Theory and Techniques* **52**, 161–169 (2004).
- [63] S. A. Schelkunoff, “A mathematical theory of linear arrays,” *Bell Syst. Tech. J.* **22**, 80–107 (1943).
- [64] M. V. Berry and N. L. Balazs, “Nonspreading wave packets,” *American Journal of Physics* **47**, 264–267 (1979).
- [65] G. A. Siviloglou and D. N. Christodoulides, “Accelerating finite energy Airy Beams,” *Optics Letters* **32**, 979–981 (2007).
- [66] G. A. Siviloglou, J. Broky, A. Dogariu, and D. N. Christodoulides, “Observation of accelerating airy beams,” *Physical Review Letters* **99**, 213901 (2007).
- [67] Y. Hu, G. A. Siviloglou, P. Zhang, N. K. Efremidis, D. N. Christodoulides, and Z. Chen, “Self-accelerating airy beams: Generation, control, and applications,” in *Nonlinear Photonics and Novel Optical Phenomena*, edited by Z. Chen and R. Morandotti (Springer, New York, 2012).
- [68] J. Durnin, “Exact solutions for nondiffracting beams. I. The scalar theory,” *Journal of the Optical Society of America A* **4**, 651–654 (1987).
- [69] J. Durnin, J. J. Miceli, and J. H. Eberly, “Diffraction-free beams,” *Physical Review Letters* **58**, 1499–1501 (1987).
- [70] D. McGloin and K. Dholakia, “Bessel beams: diffraction in a new light,” *Contemporary Physics* **46**, 15–28 (2005).
- [71] M. Ettore, S. M. Rudolph, and A. Grbic, “Generation of propagating bessel beams using leaky-wave modes: experimental validation,” *IEEE Trans. on Antennas and Propagation* **60**, 2645–2653 (2012).
- [72] M. Rahm, S. A. Cummer, D. Schurig, J. B. Pendry, and D. R. Smith, “Optical design of reflectionless complex media by finite embedded coordinate transformations,” *Physical Review Letters* **100**, 063903 (2008).
- [73] Y. Ke, W. Shu, H. Luo, S. Wen, and D. Fan, “Method for arbitrary phase transformation by a slab based on transformation optics and the principle of equal optical path,” *J. Europ. Opt. Soc. Rap. Publ.* **7**, 12013 (2012).